

Study of Nitrification and Denitrification in the High Ammonia and COD Load of Industrial Wastewater using an Ultracompacted Biofilm Reactor-Moving Bed System

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Abstract

Removing nitrogen, one of the most common and abundant pollutants of surface and ground water, is very important. For this purpose, biological nitrification and denitrification as the most economical method should be considered. The feasibility of high load COD (Chemical Oxygen Demand) (800-2000 mg/lit) and NH₄ (250-1000 mg/lit) industrial wastewater treatment, at different Hydraulic Retention Times (HRTs), was studied in 9-lit anaerobic-aerobic systems in the post-denitrification mode. The Ultracompacted Biofilm Reactor (UCBR) is a new system, with all the advantages of activated sludge and fluidized fixed bed processes, without the disadvantages of each system, so that the biofilm production takes place on the packings, moving along the height of the reactor. From the experiments carried out using this system, it can be said that higher ammonia removals take place at higher ammonia and lower organic loads. Denitrification increases at higher nitrification rates because of the effect increasing of NO₃ entering to anaerobic reactor. Despite the fact that nitrifying bacteria are more sensitive than COD and NO₃ for removing bacteria, after toxic shock by phenol as an organic source, the nitrification rate increases and COD removal decreases according to the damaging effect of phenol on COD-removing bacteria. Total COD removal during the study varied between 70-98%, this value changing between 50-90% for ammonia and 55-90% for nitrate.

Keywords: Industrial wast water, Denitrification, Nitrification, Ultracompacted Biofilm Reactor(UCBR).

مطالعات یک بیورآکتور با بستر متراکم به منظور حذف نیترات در پسابهای صنعتی

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حكيده

کلیدواژهها: پساب صنعتی، دی نیتریفیکاسیون، نیتریفیکاسیون، پیورآکتور با بستر متراکم.

Introduction

Biological nitrification and denitrification processes are the most important wastewater treatment processes because of the abundance of nitrogen pollutant compounds in water and wastewater and also because of the growing trend in population and the increasing number of industrial plants and agricultural fields, especially in developing countries.

It is generally believed, on a relative basis, that ammonia and nitrite oxidation is carried out mainly by autotrophs of the types Nitrosomonase sp. And Nitrobacter sp.

A few features of the autotrophic Nitrifying bacteria, Nitrosomonase and Nitrobacter are summarized in Table 1. In denitrification, nitrite reduction to N2 is carried out by heterotrops of the Psudomonase.

One potential biofilm process, which may be compact, is the one based on submerged biological filters. There are many reports concerning the possibility of using biofilm processes for treating wastewater (MBBr, 2000; Carrera et al., 2003; ong et al., 2003; chen et al., 1995; Halling- sarenson and Jorgensen, 1993) but the disadvantage of some biological filters is the possibility of clogging of the biofilm media (MBBr, 2000; carrera et al., 2003, ong et al., 2003; chen et al., 1995; Rusten et al., 1994; Rusten et al., 1996).

The biofilm process in the Ultracompacted Biofilm Reactor (UCBR) has a high specific surface, but none of the clogging (Al- Ghusain, 1994). In this reactor, the biofilm grows on carriers circulating inside the tank. The carriers are shaped to maximize growth, by protecting the biofilm from abrasion (Van loosdrecht et al., 1995; carrera et al., 2003).

The First and best study on (UCBR) process was developed by Ong, Lee, Hu and Ng at the National University of Singapore on January 2003 (Al-Ghusain, 1994). The basic idea behind the (UCBR) in this research was to have a batch operating, with a non-cloggable biofilm reactor with no need for backwashing, low-loss and a high specific biofilm

surface area(Al- Ghusain, 1994). This reactor is becoming increasingly popular and is now being used in many plants around the world for various treatment purposes (BOD/COD removal, nitrification and denitrification) in both municipal and industrial wastewater (yang and zhang, 1995).

This paper examines the results obtained from two pilot anaerobic-aerobic (UCBR)-(MBS) plants in their application to both organic carbon and nitrogen removal.

Table 1- Characteristics of Nitrosomonase and Nitrobacter

| | Nitrosomonase | Nitrobacter |
|---------------------------------|---------------------------|-----------------------------|
| Morphology | Rod-shaped | Rod-shaped |
| Cell size | 1*10-6 by 1.5*10-6 (m) | 0.5 *10-6 by 1*10- 6 (m) |
| Gram Test | Negative | Negative |
| Mobile | May or may not be | May or may not |
| Autotroph | Obligate | Facultative |
| Dissolved Oxygen Requirement | Strict Aerobic | Strict Aerobic |
| Optimum Temperature | 5-35 (0 c) | 5-35 (0 c) |
| Optimum p H | 7.8-9.2 | 8.2-9.2 |
| Estimated Generation Time | 8-36 (hr) | 12-59 (hr) |
| Free-Energy Efficiency | 11-27 | 34 |

Materials and Methods

The technical and operating data as well as a simplified figure and flowsheet of the pilot plant are shown in Table 2, Figure 1 and Figure 2 respectively. The pilot plant was operated in the post-denitrification mode, with two reactors in use. The first reactor was always aerobic and the second one was anaerobic. The process was based on the biofilm principle and the biomass grew on small elements that move along with the wastewater in reactor.

The movement was typically produced by coarse bubble aeration in aerobic and mechanical mixing in an anaerobic reactor. The biofilm carrier elements were made of 0.9 specific gravity of polyethylene, about 13 mm long and 13.5 mm in diameter. The aerobic reactor was filled to 80% volume and the Anaerobic reactor was filled to 60% volume, providing a specific surface area equal to 192.5 m²/m³. As shown in Figures 1 and 2, two anaerobic- aerobic reactors were operated in post-denitrification mode to study the feasibility of treating high ammonia and COD load wastewater without spending extra expense to add an external carbon source and to provide high C/N ratio for the denitrification process.

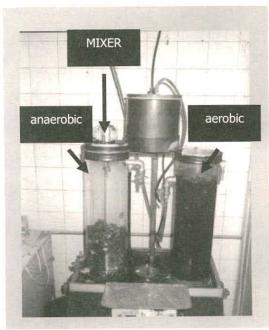


Figure 1- The two anaerobic- aerobic reactors

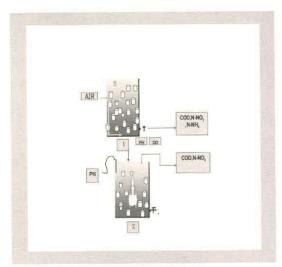


Figure 2- Flowsheet of the two reactors

This configuration also helps to reduce influent COD to the denitrification reactor.

The technical and operating data of the pilot plant are given in Table 2.

Table 2- Technical and Operating data for UCBR and MBS

| Technical Dates | Feed Tank | UCBR | MBS |
|----------------------|-----------------|------------------|----------------------|
| Hight | 62 cm | 55 cm | 55cm |
| Diameter | 33 cm | 15 cm | 15 cm |
| Volume | 50 lit | 9 lit | 9/1 lit |
| Shaft Height | | | 48 cm |
| Impeller Diameter | innexmon | 10 cm | 10 cm |
| Filling Ratio | 355571327113771 | 80% | 60% |
| Electromotor | | | DC,5 Amp.,40 Voli |
| Aeration | *********** | Coarse Bubble | |

A water lock was located above denitrification reactor and any biogas exiting from anaerobic reactor passes through a water column and exits from a water lock to prevent air entering the anaerobic reactor.

These experiments were carried out to study the effect of HRT, COD load and NH₄⁺ load on nitrification and denitrification rate in 2-20 HRTs, two COD loads in each HRT and variable ammonia concentrations for each COD load. The process was

tested in a pilot plant for the treatment of a high ammonia and COD load. The composition of the synthetic wastewater is: (NH₄-N: 250-1000 (mg/lit), COD: 800-1500 (mg/lit),). NH₄HCO₃ and NH₄CL were used as the ammonia sources and phosphorous was provided by adding KH₂PO₄, NH₄HCO₃ and KH2PO₄ which were chosen as buffer compounds to control the pH of process. Micronutrients such as Cu,Cl,Mg,Na,and Fe were added to the system as CuSO₄ (2 mg/lit), MgSO₄ (3 mg/lit), FeCl₃ (0.4 mg/lit), and NaCl (0.7 mg/lit).

This wastewater consisted of: 764.2mg/l ammonium chloride,1029.4mg/l sodium acetate, 1200mg/l sodium bicarbonate,28.1mg/l di-potassium hydrogen phosphate and 1mg/l of trace element solution. Each liter of trace element solution contained 10g calcium chloride, 8g ferric chloride, 5g magnesium sulphate, 2g cobalt chloride, 2g thiamine-HCL, 1g sodium silicate, 550mg aluminum sulphate, 50mg manganese chloride, 1mg ammonium molybdate, 1mg copper sulphate, 1mg zinc sulphate and 1mg boric acid (Table 3).

Temperature and pH were measured in each bioreactor every working day, immediately before sampling. The influent wastewater and the content of the UCBR and MBS at the end of aerobic and anaerobic reactors were sampled everyday. The samples were analysed immediately after sampling to obtain the parameters shown in Table 4 and 5. The parameters were measured according to the Standard Methods (1992) (Halling- sorensen and Jorgensen, 1993).

Results

Batch Operation

The experiment was aimed at studying the behavior of the MBBR for COD removal and also simultaneous nitrification and denitrification during the aerobic and anaerobic stages. The batch operation was used as a start-up for the growth of biofilm on packing. After this period, the biofilm appeared on the packing elements and UCBR appeared to be ready for batch operation. Characteristics of the initial aerobic and anaerobic wastewater are given in Table 6.

di-potassium hydrogen phosphate Trace elements ammonium chloride sodium bicarbonate sodium acetate mg/l ammonium molybdate magnesium sulphate manganese chloride aluminum sulphate calcium chloride copper sulphate ferric chloride cobalt chloride sodium silicate thiamine-HCI zinc sulphate boric acid 764.2 1079.4 1200 28 1 102 20 1g 8g 2g 550mg 50mg Img lmg lmg 1mg

Table 3- Analysis of the trace elements

Table 4- Removal rate of the ammonia in UCBR with Vari-Inf-Ammonia

| | AEROBIC- COD=800mg/l | | | | | | | | |
|----------|----------------------|----------|--------|----------|--------|----------|--------|------|----|
| R emoval | Conc | R emoval | Cone | R emoval | Conc | R emoval | Conc | R | |
| % | (mg/l) | % | (mg/l) | % | (mg/l) | % | (mg/l) | time | NO |
| 0.0 | 400 | 0.0 | 350 | 0.0 | 300 | 0.0 | 250 | 0 | 1 |
| 22.0 | 312 | 11.1 | 311 | 23.3 | 230 | 14.4 | 214 | 2 | 2 |
| 36.0 | 256 | 23,4 | 268 | 35.0 | 195 | 30.4 | 185 | 4 | 3 |
| 58.8 | 165 | 55,4 | 156 | 55.0 | 135 | 38.4 | 154 | 6 | 4 |
| 53.8 | 185 | 53.7 | 162 | 66.7 | 100 | 36.0 | 160 | 8 | 5 |
| 51.5 | 194 | 70.9 | 102 | 78.3 | 65 | 51.6 | 121 | 10 | 6 |
| 62.0 | 152 | 74.0 | 91 | 82.0 | 54 | 64.4 | 89 | 12 | 7 |
| 76.5 | 94 | 86.3 | 48 | 84.7 | 46 | 68.8 | 78 | 14 | 8 |
| 76.3 | 95 | 90.0 | 35 | 89.3 | 32 | 70.4 | 74 | 16 | 9 |
| 85.0 | 60 | 94.0 | 21 | 94.0 | 18 | 75.6 | 61 | 18 | 10 |
| 97.5 | 10 | 93.4 | 23 | 95.0 | 15 | 96.0 | 10 | 20 | 11 |
| 96.5 | 14 | 97.7 | 8 | 96.0 | 12 | 98.4 | 4 | 24 | 12 |
| 0.0 | 700 | 0.0 | 650 | 0.0 | 520 | 0.0 | 450 | 0 | 1 |
| 27.1 | 510 | 15.7 | 548 | 27.5 | 377 | 22.2 | 350 | 2 | 2 |
| 28.6 | 500 | 36.8 | 411 | 47,3 | 274 | 28.7 | 321 | 4 | 3 |
| 39.9 | 421 | 30.6 | 451 | 61.7 | 199 | 37,8 | 280 | 6 | 4 |
| 44.6 | 388 | 50.6 | 321 | 72.1 | 145 | 48.4 | 232 | 8 | 5 |
| 63.6 | 255 | 62.9 | 241 | 79.8 | 105 | 44.2 | 251 | 10 | 6 |
| 70.0 | 210 | 71.5 | 185 | 85.4 | 76 | 58.0 | 189 | 12 | 7 |
| 73.6 | 185 | 73.2 | 174 | 89.4 | 55 | 63.3 | 165 | 14 | 8 |
| 79.7 | 142 | 81.1 | 123 | 91.9 | 42 | 68.9 | 140 | 16 | 9 |
| 90.7 | 65 | 84.9 | 98 | 94.2 | 30 | 75.1 | 112 | 18 | 10 |
| 97.0 | 21 | 86.9 | 85 | 96.0 | 21 | 96.0 | 18 | 20 | 11 |
| 98.0 | 14 | 93.7 | 41 | 95.2 | 25 | 95.3 | 21 | 24 | 12 |

| | | | | AEROBIC - C | OD=800mg/ | | | | |
|--|---|---|---|---|---|--|--|------------------------------|--------------------|
| emoval | Conc | Removal | Conc | R emoval | Conc | R emoval | Conc | R | 200 |
| % | (mg/l) | % | (mg/l) | % | (mg/l) | % | (mg/l) | time | NO |
| 0.0 | 1000 | 0.0 | 900 | 0.0 | 800 | 0.0 | 750 | 0 | 1 |
| 14.5 | 855 | 19.7 | 723 | 9.9 | 721 | 3.9 | 721 | 2 | 2 |
| 28.8 | 712 | 33.3 | 600 | 12.5 | 700 | 13.2 | 651 | 4 | 3 |
| 64.5 | 355 | 54.3 | 411 | 33.4 | 533 | 29.1 | 532 | 6 | 4 |
| 71.5 | 285 | 75.3 | 222 | 48.6 | 411 | 40.8 | 444 | 8 | 5 |
| 75.8 | 242 | 71.8 | 254 | 62.3 | 302 | 57.1 | 322 | 10 | 6 |
| 80.0 | 200 | 80.7 | 174 | 59.8 | 322 | 53.1 | 352 | 12 | 7 |
| 89.6 | 104 | 87.7 | 111 | 64.4 | 285 | 63.3 | 275 | 14 | 8 |
| 91.5 | 85 | 86,3 | 123 | 73.8 | 210 | 71.3 | 215 | 16 | 9 |
| 94.0 | 60 | 95,1 | 44 | 86.1 | 111 | 78.0 | 165 | 18 | 10 |
| | | 30.00 | | 95.9 | 33 | 91.7 | 62 | 20 | 11 |
| 96.0 | 40 | 92.7 | 66 | 95.9 | :33 | 91.7 | 02 | 20 | 11 |
| | | | | | | | | | |
| 95.4 | 46 | 98.7 | 12 | 93.9 | 49 | 96.9 | 23 | 24 | 12 |
| 95.4 | 46 | 98.7 | 12 | 93.9 AEROBIC-CO | | | 23 | 24 | 12 |
| 95.4 Removal | 46 Cone | 98.7 Removal | 12 Conc | 5 5 50 | | | Conc | 24 R | |
| | | | | AEROBIC-CO | OD=1500mg/ | | | | NO NO |
| Removal | Conc | Removal | Conc | AEROBIC- CO | OD=1500mg/ Conc | Removal | Conc | R | |
| Removal | Conc (mg/l) | Removal | Conc (mg/l) | AEROBIC- CO | Conc (mg/l) | Removal | Conc (mg/l) | R time | NO |
| Removal % 0.0 | Conc (mg/l) | Removal % 0.0 | Conc (mg/l) 350 | AEROBIC-CO | Conc (mg/l) 300 | Removal % | Conc (mg/l) 250 | R time | NO 1 |
| % 0.0 10.0 | Conc (mg/l) 400 360 | Removal % 0.0 | Conc (mg/l) 350 322 | Removal % 0.0 23.3 | Conc (mg/l) 300 230 | Removal % 0.0 12.0 | Cone (mg/l) 250 220 | R time | NO 1 |
| % 0.0 10.0 17.5 | Conc (mg/l) 400 360 330 | Removal % 0.0 8.0 18.6 | Conc (mg/l) 350 322 285 | AEROBIC-CO Removal % 0.0 23.3 30.0 | Conc (mg/l) 300 230 210 | Removal % 0.0 12.0 25.0 | Conc (mg/l) 250 220 | R time 0 2 | NO 1 2 3 |
| % 0.0 10.0 17.5 61.3 | Conc (mg/l) 400 360 330 | Removal % 0.0 8.0 18.6 40.0 | Conc (mg/l) 350 322 285 210 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 | Conc (mg/l) 300 230 210 | Removal % 0.0 12.0 25.0 38.4 | Conc (mg/l) 250 220 195 | R time 0 2 4 | NO 1 2 3 4 |
| Removal % 0.0 10.0 17.5 61.3 53.8 | Conc (mg/l) 400 360 330 155 | Removal % 0.0 8.0 18.6 40.0 27.1 | Conc (mg/l) 350 322 285 210 255 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 66.0 | Conc (mg/l) 300 230 210 145 | Removal % 0.0 12.0 25.0 38.4 | Conc (mg/l) 250 220 195 154 | R time 0 2 4 6 | NO 1 2 3 4 5 |
| Removal % 0.0 10.0 17.5 61.3 53.8 49.5 | Conc (mg/l) 400 360 330 155 185 | Removal % 0.0 8.0 18.6 40.0 27.1 | Conc (mg/l) 350 322 285 210 255 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 66.0 | Conc (mg/l) 300 230 210 145 102 | Removal % 0.0 12.0 25.0 38.4 32.0 46.4 | Conc (mg/l) 250 220 195 154 170 | R time 0 2 4 6 8 | NO 1 2 3 4 5 |
| Removal % 0.0 10.0 17.5 61.3 53.8 49.5 58.8 | Conc (mg/l) 400 360 330 155 185 202 | Removal % 0.0 8.0 18.6 40.0 27.1 65.4 71.4 | Conc (mg/l) 350 322 285 210 255 121 100 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 66.0 71.7 78.3 | Conc (mg/l) 300 230 210 145 102 85 | Removal % 0.0 12.0 25.0 38.4 32.0 46.4 64.0 | Conc (mg/l) 250 220 195 154 170 134 | R time 0 2 4 6 8 10 | NO 1 2 3 4 5 6 |
| Removal % 0.0 10.0 17.5 61.3 53.8 49.5 58.8 | Conc (mg/l) 400 360 330 155 185 202 165 | Removal % 0.0 8.0 18.6 40.0 27.1 65.4 71.4 86.3 | Conc (mg/l) 350 322 285 210 255 121 100 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 66.0 71.7 78.3 | Conc (mg/l) 300 230 210 145 102 85 65 | Removal % 0.0 12.0 25.0 38.4 32.0 46.4 64.0 | Conc (mg/l) 250 220 195 154 170 134 90 | R time 0 2 4 6 8 10 12 | NO 1 2 3 4 5 6 7 |
| Removal % 0.0 10.0 17.5 61.3 53.8 49.5 58.8 75.0 | Conc (mg/l) 400 360 330 155 185 202 165 100 103 | Removal % 0.0 8.0 18.6 40.0 27.1 65.4 71.4 86.3 | Conc (mg/l) 350 322 285 210 255 121 100 48 | AEROBIC-CO Removal % 0.0 23.3 30.0 51.7 66.0 71.7 78.3 78.0 | Conc (mg/l) 300 230 210 145 102 85 65 66 45 | Removal % 0.0 12.0 25.0 38.4 32.0 46.4 64.0 68.8 | Conc (mg/l) 250 220 195 154 170 134 90 78 | R time 0 2 4 6 8 10 12 14 16 | NO 1 2 3 4 5 6 7 8 |

| Removal | Conc | Removal | Conc | Removal | Conc | Removal | Conc | R | NO |
|--|---|--|--|---|---|--|---|---------------------------------|-------------------------|
| % | (mg/l) | % | (mg/l) | % | (mg/l) | % | (mg/l) | time | NO |
| 0.0 | 700 | 0.0 | 650 | 0.0 | 520 | 0.0 | 450 | 0 | 1 |
| 5.7 | 660 | 2.2 | 636 | 8.3 | 477 | 2.2 | 440 | 2 | 2 |
| 35.6 | 451 | 25.4 | 485 | 38.1 | 322 | 11.6 | 398 | 4 | 3 |
| 39.9 | 421 | 24.9 | 488 | 59.4 | 211 | 21.1 | 355 | 6 | 4 |
| 43.0 | 399 | 43.8 | 365 | 73.1 | 140 | 28.7 | 321 | 8 | 5 |
| 63.6 | 255 | 56.2 | 285 | 68.3 | 165 | 40.4 | 268 | 10 | 6 |
| 67.9 | 225 | 67.5 | 211 | 83.1 | 88 | 55.1 | 202 | 12 | 7 |
| 70.0 | 210 | 69.2 | 200 | 85.2 | 77 | 57.8 | 190 | 14 | 8 |
| 76.4 | 165 | 76.0 | 156 | 87.5 | 65 | 57.3 | 192 | 16 | 9 |
| 89.3 | 75 | 83.2 | 109 | 92.7 | 38 | 63.1 | 166 | 18 | 10 |
| 95.3 | 33 | 84.8 | 99 | 95.6 | 23 | 81.1 | 85 | 20 | 11 |
| 96.9 | 22 | 90.0 | 65 | 96.2 | 20 | 85.6 | 65 | 24 | 12 |
| | | | | AEROBIC- C | OD=1500mg/ | 1 | | | |
| | | | | | | | | | |
| Removal | Conc | Removal | Conc | Removal | Conc | Removal | Conc | R | |
| | Conc (mg/l) | Removal | Conc (mg/l) | Removal | Cone (mg/l) | Removal | | 10 | NO |
| % | (mg/l) | % | (mg/l) | % | (mg/l) | % | (mg/l) | time | |
| | | | | | | | | 10 | NO 1 |
| % | (mg/l) | % | (mg/l) | % | (mg/l) | % | (mg/l) | time | |
| 0.0 | (mg/l) 1000 | % 0.0 | (mg/l) 900 | 0.0 | (mg/l) 800 | % 0.0 | (mg/l) 750 | time 0 | 1 |
| % 0.0 1.0 | (mg/l) 1000 | % 0.0 5.0 | (mg/l) 900 855 | 0.0 | (mg/l) 800 777 | % 0.0 3.9 | (mg/l) 750 721 | time 0 2 | 1 2 |
| % 0.0 1.0 23.5 | (mg/l) 1000 990 765 | % 0.0 5.0 22.3 | (mg/l) 900 855 699 | % 0.0 2.9 | (mg/l) 800 777 700 | % 0.0 3.9 | 750 721 651 | time 0 2 4 | 2 3 |
| % 0.0 1.0 23.5 64.5 | (mg/l) 1000 990 765 355 | % 0.0 5.0 22.3 42.1 | (mg/l) 900 855 699 521 | % 0.0 2.9 12.5 | (mg/l) 800 777 700 655 | % 0.0 3.9 13.2 26.0 | (mg/l) 750 721 651 555 | time 0 2 4 6 | 3 |
| % 0.0 1.0 23.5 64.5 | (mg/l) 1000 990 765 355 544 | % 0.0 5.0 22.3 42.1 64.2 | (mg/l) 900 855 699 521 322 | % 0.0 2.9 12.5 18.1 47.4 | (mg/l) 800 777 700 655 421 | % 0.0 3.9 13.2 26.0 | (mg/l) 750 721 651 555 444 | time 0 2 4 6 | 3 4 5 |
| % 0.0 1.0 23.5 64.5 45.6 | (mg/l) 1000 990 765 355 544 322 | % 0.0 5.0 22.3 42.1 64.2 70.6 | (mg/l) 900 855 699 521 322 265 | % 0.0 2.9 12.5 18.1 47.4 61.3 | (mg/l) 800 777 700 655 421 310 | % 0.0 3.9 13.2 26.0 40.8 51.3 | (mg/l) 750 721 651 555 444 365 | time 0 2 4 6 8 10 | 1 2 3 4 5 5 6 |
| % 0.0 1.0 23.5 64.5 45.6 67.8 | (mg/l) 1000 990 765 355 544 322 265 | % 0.0 5.0 22.3 42.1 64.2 70.6 79.4 | (mg/l) 900 855 699 521 322 265 | % 0.0 2.9 12.5 18.1 47.4 61.3 59.8 | (mg/l) 800 777 700 655 421 310 322 | % 0.0 3.9 13.2 26.0 40.8 51.3 | (mg/l) 750 721 651 555 444 365 | time 0 2 4 6 8 10 | 1 2 3 4 5 5 6 7 |
| % 0.0 1.0 23.5 64.5 45.6 67.8 73.5 83.5 | (mg/l) 1000 990 765 355 544 322 265 | % 0.0 5.0 22.3 42.1 64.2 70.6 79.4 | (mg/l) 900 855 699 521 322 265 185 | % 0.0 2.9 12.5 18.1 47.4 61.3 59.8 | (mg/l) 800 777 700 655 421 310 322 285 | % 0.0 3.9 13.2 26.0 40.8 51.3 51.7 60.1 | (mg/l) 750 721 651 555 444 365 362 299 | time 0 2 4 6 8 10 12 | 1 2 3 4 5 6 7 8 8 |
| % 0.0 1.0 23.5 64.5 67.8 73.5 83.5 89.9 | (mg/l) 1000 990 765 355 544 322 265 165 | % 0.0 5.0 22.3 42.1 64.2 70.6 79.4 70.6 85.0 | (mg/l) 900 855 699 521 322 265 185 265 | % 0.0 2.9 12.5 18.1 47.4 61.3 59.8 64.4 75.0 | (mg/l) 800 777 700 655 421 310 322 285 200 | % 0.0 3.9 13.2 26.0 40.8 51.3 51.7 60.1 61.6 | (mg/l) 750 721 651 555 444 365 362 299 288 | time 0 2 4 6 8 10 12 14 | 1 2 3 4 5 5 6 7 7 8 8 9 |

Table 5- Removal rate of nitrate in the MBS with Vari-influent-Nitrate

| Action Control of | | P . | | | 0 | I m | 0 | | T. ST. |
|-------------------------------------|------------------------------------|-------------------------------------|--|---|-------------------------------------|---------------------------------------|-----------------------------------|---------------------|----------------------------|
| Removal % | Conce (mg/l) | Removal | Conce (mg/l) | Removal | Conc (mg/l) | Removal | Conc (mg/l) | R Time | NO |
| 0.0 | 600 | 0.0 | 507 | 0.0 | 400 | 0.0 | 250 | 0 | 1 |
| 25.0 | 450 | 19.7 | 407 | 25.0 | 300 | 20.0 | 200 | 2 | 2 |
| 29.8 | 421 | 35.7 | 326 | 37.5 | 250 | 44.0 | 162 | 4 | 3 |
| 53.3 | 280 | 48.3 | 262 | 59.5 | 162 | 51.6 | 121 | 6 | 4 |
| 57.5 | 255 | 58.6 | 210 | 59.5 | 162 | 55.2 | 112 | 8 | 5 |
| 66.7 | 200 | 66.7 | 169 | 72.3 | 111 | 59.2 | 102 | 10 | 6 |
| 81.7 | 110 | 73.4 | 135 | 73.0 | 108 | 77.6 | 56 | 12 | 7 |
| 83.3 | 100 | 83.2 | 85 | 82.5 | 70 | 83.2 | 42 | 14 | 8 |
| 76.7 | 140 | 83.2 | 85 | 82.3 | 71 | 82.8 | 43 | 16 | 9 |
| 81.3 | 112 | 86.2 | 70 | 80.0 | 80 | 84.4 | 39 | 18 | 10 |
| | | | | | | | | | |
| | | JE STEEL | A | NAEROBIC- | COD=1500n | ng/I | TENT | | |
| Pamoval | Cons | Pomoval | | | | | Conc | P | |
| Removal | Conc (mg/l) | Removal | Conc (mg/l) | Removal % | COD=1500n Conc (mg/l) | ng/l Removal | Conc (mg/l) | R Time | NO |
| | | 13. | Conc | Removal | Conc | Removal | 27 (200 | 1000 | NO 1 |
| % | (mg/l) | % | Conc (mg/l) | Removal | Conc (mg/l) | Removal | (mg/l) | Time | |
| % 0.0 | (mg/l) 600 | 0.0 | Conc (mg/l) 507 | Removal % | Conc (mg/l) 400 | Removal % | (mg/l) 250 | Time 0 | 1 |
| 0.0 | (mg/l) 600 488 | 0.0 | Conc (mg/l) 507 | Removal % 0.0 19.5 | Conc (mg/l) 400 | Removal % 0.0 2.0 | (mg/l) 250 245 | Time 0 2 | 1 2 |
| % 0.0 18.7 22.0 | (mg/l) 600 488 468 | % 0.0 18.7 27.8 | Conc (mg/l) 507 412 366 | Removal % 0.0 19.5 22.5 | Conc (mg/l) 400 322 310 | Removal % 0.0 2.0 20.8 | (mg/l) 250 245 199 | Time 0 2 4 | 2 |
| % 0.0 18.7 22.0 50.0 | (mg/l) 600 488 468 300 | % 0.0 18.7 27.8 48.3 | Conc (mg/l) 507 412 366 262 | Removal % 0.0 19.5 22.5 58.8 | Conc (mg/l) 400 322 310 | Removal % 0.0 2.0 20.8 38.0 | (mg/l) 250 245 199 | Time 0 2 4 6 | 3 |
| % 0.0 18.7 22.0 50.0 55.8 | (mg/l) 600 488 468 300 265 | % 0.0 18.7 27.8 48.3 49.9 | Conc (mg/l) 507 412 366 262 254 | Removal % 0.0 19.5 22.5 58.8 59.5 | Conc (mg/l) 400 322 310 165 | Removal % 0.0 2.0 20.8 38.0 51.6 | (mg/l) 250 245 199 155 | Time 0 2 4 6 8 | 1 2 3 4 |
| % 0.0 18.7 22.0 50.0 55.8 65.0 | (mg/l) 600 488 468 300 265 | % 0.0 18.7 27.8 48.3 49.9 60.9 | Conc (mg/l) 507 412 366 262 254 | Removal % 0.0 19.5 22.5 58.8 59.5 68.8 | Conc (mg/l) 400 322 310 165 162 | Removal % 0.0 2.0 20.8 38.0 51.6 42.0 | (mg/l) 250 245 199 155 121 | Time 0 2 4 6 8 10 | 1 2 3 4 5 |
| % 0.0 18.7 22.0 50.0 55.8 65.0 81.5 | (mg/l) 600 488 468 300 265 210 | % 0.0 18.7 27.8 48.3 49.9 60.9 75.3 | Conc (mg/l) 507 412 366 262 254 198 | Removal % 0.0 19.5 22.5 58.8 59.5 68.8 72.5 | Conc (mg/l) 400 322 310 165 162 125 | Removal % 0.0 2.0 20.8 38.0 51.6 42.0 | (mg/l) 250 245 199 155 121 145 66 | Time 0 2 4 6 8 10 | 1 2 3 4 5 6 |

Table 6- Characteristics of initial wastewater in both systems

| Parameter | Aerobic UCBR | Anaerobie MBS |
|---------------------------------------|--------------|---------------|
| COD(mg/lit) | 800 | 200 |
| NH ₄ ⁺ (mg/lit) | - 520 | 22 |
| NO ₃ (mg/lit) | 350 | 475 |
| PH | 6/6-7/9 | 6/1-7/7 |

For a period of 160 days, the pilot plant was operated and the experimental results for different HRTs, COD and nitrogen-loading rates are shown in Figure 3 to Figure 6.

 Because of the high concentration of nitrates in the effluent, the Hydraulic Retention Time (HRT) was increased to 24hr.

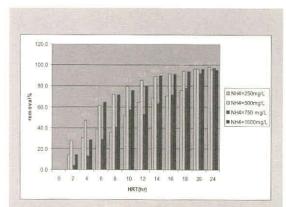


Figure 3- Ammonia removal at different HRTs in the aerated tank

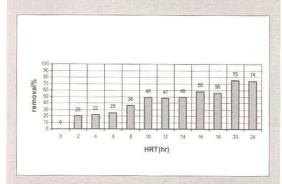


Figure 4- COD removal at different HRTs in the aerobic tank

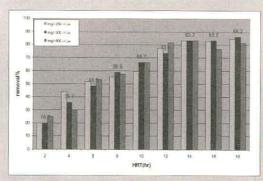


Figure 5- Nitrate removal at different HRTs in the anaerobic tank

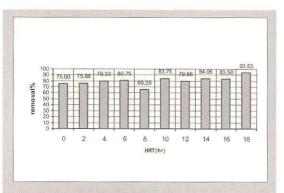


Figure 6- COD removal at different HRTs in the anaerobic tank

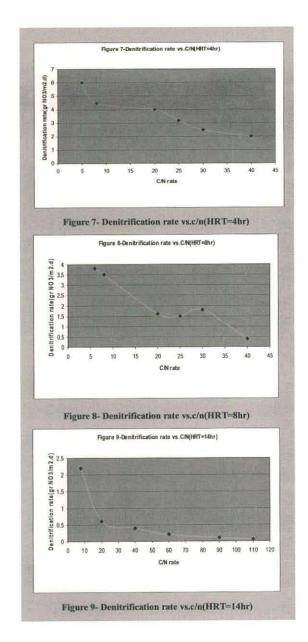
Discussion

As shown in Figures 3 to 6, the nitrification and denitrification rate increases when HRT increases. It can be concluded that the competitive inhibition effect at high COD loads influenced the nitrifier bacteria, which compete with carbonaceous bacteria at high COD loading rates. At higher ammonia loads it is easier for nitrifiers to compete with the other microorganisms, to consume the dissolved oxygen in system.

The nitrification rate has a dual effect on COD removal. On the one hand, COD removal increases when a high nitrification rate occurs because of the higher activity of the nitrifiers. On the other hand, when the nitrification rate increases, more nitrate enters the anaerobic reactor and, as a result, more denitrification and subsequently more COD removal occurs. The effect of nitrate concentration on denitrification rate is shown in Figure 5.

An another important result obtained is that the influence of nitrate concentration is more important than the C/N ratio which has been regarded as one of the most important factors on the denitrification rate.(see Figure 7 to Figure 9)

The other results show the low sensivity of the UCBR to HRT and the insignificant effect of HRT change on COD removal and the denitrification and nitrification process, showing the high stability of the UCBR.



Conclusions

From the different tests in pilot-scale plants, the following experiences have been gained with UCBR-MBS:

- The reactor has demonstrated its capability for he nitrification, denitrification and organic removal process for a broad range of ammonia and COD.
- The major advantages of UCBR as compared to other systems are its simplicity in operation, low space requirement, stability, reliability, good settlability, low

head loss, no bulking and lack of bachwash requirement.

- The percentage of COD removal did not fall below 75% and was most of the time more than 85%.
- 4) The percentage of ammonia removal was mostly more than 95% at 20 hr and the nitrate removal percentage above 80% at 14 hr.
- 5) The percentage of COD removal was more than 75% at 20 hr in aerobic tank and above 80% at 14 hr in an anaerobic tank.

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